

		実施例				比較例		
		ロ-1	ロ-2	ロ-3	ロ-4	ロ-5	ロ-6	ロ-7
混合物 (1) (b-1)	(部)	60	65	85	45	60	65	85
	MMA (%)	30	45	15	55	30	45	15
	B A (%)	70	55	85	45	70	55	85
	BDMA (%)	0.70	0.90	2.00	0.45	0.70	0.90	2.00
	BPO (%)	0.02	0.01	0.04	0.02	0.02	0.01	0.04
混合物 (2) (b-1) → (B)	(部)	40	35	15	55	40	35	15
	MMA (部)	90	80	95	85	90	80	95
	B A (部)	10	20	5	15	10	20	5
	BPO (部)	0.03	0.01	0.02	0.02	0.03	0.01	0.02
架橋アクリル酸エステル系重合体 (b-1) の ゲル含有率 (%)		90	93	99	95	90	93	99
アクリル系グラフト共重合体 (B) の 重量平均粒子径 (μm)		5	3	7	13	5	3	7
分級の有無		有	有	有	有	無	無	無
60 μm以上の粒子の含有率 (重量%)		0	0	0	0	8	5	10

(3) 熱可塑性樹脂組成物の製造 実施例ハ 1~7、

比較例ハ 8~11

表3に示すアクリル樹脂(A)とアクリル系グラフト共重合体(B)をヘンシェルミキサーで混合した。この混合物をペント式押出機で190℃設定で押し出し、ペレット化し、前記した物性、特性の測定、評価に供した。

尚、ペレット中の残存セブマーは500ppm以下であった。該ペレットをT型ダイス付き押出機でフィルムに成形し、前記した物性、特性の測定、評価に供した。

【0062】

【表3】

	実施例							比較例			
	ハ-1	ハ-2	ハ-3	ハ-4	ハ-5	ハ-6	ハ-7	ハ-8	ハ-9	ハ-10	ハ-11
多層構造を有するアクリル樹脂 (A) (数値)	イ-1	100			100			100			
	イ-2		100				100		100	100	
	イ-3			100							
	イ-4				100						100
アクリル系グラフト共重合体 (B) (数値)	ロ-1	6							70		
	ロ-2		8								
	ロ-3			5							
	ロ-4				5						
	ロ-5				2			6			6
	ロ-6					10					
	ロ-7						8			8	
30℃での金属ロール押さえつけ											
メルトインデックス	6.5	6.3	5.3	8.0	6.8	6.0	6.2	6.5	1.5	6.2	8.0
耐衝撃性	11.8	9.8	14.7	6.9	13.7	8.8	10.8	11.8	2.9	10.8	6.9
ビカット	71	70	68	75	70	73	71	71	58	71	75
透明性	90	87	88	90	93	88	89	90	51	89	91
	45	40	43	47	35	44	41	45	70	41	43
光沢	30	28	34	35	45	27	33	30	10	33	35
耐溶剤性	60	65	60	70	58	52	50	60	65	50	60
耐可塑剤移行性	20	21	19	12	20	24	22	20	48	22	18
折曲白化性	○	○	○	○	○	○	○	○	×	○	○
加工性	○	○	○	○	○	○	○	○	×	○	○
印刷抜け	0.1	0.5	2.3	1.0	2.3	1.1	2.0	40.0	80.0	50.0	40.0
片面性	○	○	○	○	○	○	○	○	×	○	○

【0063】

【発明の効果】表3から明らかなように、実施例で代表される本発明の艶消し熱可塑性樹脂フィルムは、折曲白

化性、耐衝撃性、耐溶剤性、耐可塑剤移行性に優れ、フィッシュアイ等のごときフィルム表面の凸部を減少させることにより表面性に優れ、印刷抜けを起こさない。

diat frequency (IF frequency). Tuner 102 selects a particular RF signal under control of a tuner control unit 104. Alternatively, tuner control unit 104 may also be included within tuner 102. Tuner control unit 104 applies a tuning control signal to tuner 102 via a wire 103, and applies bandswitching signals via a control bus 103'. The tuning control signal and bandswitching signals control the frequency at which local oscillator 102c oscillates, thus determining which RF signal is converted (heterodyned) to the IF frequency. Tuner control unit 104 is controlled by a controller 110. Controller 110, which may be a microprocessor or microcomputer, includes a central processing unit (CPU) 112, a read-only memory (ROM) 114, and a random access memory 116. Controller 110 receives user-entered control signals from a local keyboard 122, and from an infrared (IR) receiver 120. IR receiver 120 receives and decodes remote control signals transmitted by a remote control unit 125.

The intermediate frequency (IF) signal produced by tuner 102 is applied to a surface acoustic wave (SAW) filter preamplifier 105 which amplifies the IF signal and applies it, via SAW filter 106 to a video signal processing unit 130. Video signal processing unit 130 comprises a video IF (VIF) amplifying stage, an automatic gain control circuit (AGC), an automatic fine tuning circuit (AFT), a video detector, and a sound IF (SIF) amplifying stage. Processing unit 130 produces a baseband composite video signal (TV), and a sound carrier signal. The sound carrier signal is applied to an audio signal processor unit 135 which includes a TV stereo decoder, a matrix, and a DBX expander. Audio signal processor unit 135 produces left and right audio signals and applies them to one pair of inputs of an audio switch unit 136. The output of audio switch unit 136 is coupled to an audio amplifier unit 137. Audio amplifier unit 137 produces amplified baseband left and right audio signals and applies them to a pair of speakers 138 for sound reproduction.

The baseband video signal (TV) is coupled to a video processor unit 155 and a kine driver amplifier 156, and ultimately displayed on a display screen of a display device 158. Video signals are also applied to a sync separator unit 160 which derives vertical and horizontal synchronizing signals therefrom. The derived vertical and horizontal signals are applied to a deflection unit 170 for the production of deflection signals for application to the yoke assembly of display device 158. Under control of controller 110, an on-screen display processor 140 generates character signals, and applies them to a second input of video signal processor 155, for display on display device 158. The circuitry described thus far, with the exception of the particular FM trap shown in FIGURE 1, is known from the RCA CTC 156 color television chassis.

The intermediate frequency (IF) signal produced by tuner 102 is also applied, via a 43.3 Mhz bandpass filter and 48.65 MHz trap arrangement 145, to a single chip FM radio integrated circuit (IC) 180. FM radio IC 180 is, for example, a CXA12338M/S AM/FM Stereo Radio Circuit manufactured by SONY Corporation. FM radio IC 180 includes an amplifier 180a, a mixer 180b, an oscillator 180c, a voltage controlled oscillator (VCO) 180d, an FM IF and detector unit 180e, and an FM stereo decoder unit 180f.

It is herein recognized that television tuner 102 may be used as the first frequency conversion stage of a double conversion tuner for the FM broadcast band, wherein the second frequency conversion stage of the double conversion tuner is provided by FM radio IC 180. That is, a particular FM radio signal is selected and converted in frequency from one of the FM radio band of frequencies, to a first intermediate frequency of 43.3 MHz. The value 43.3 MHz is important and its selection will be discussed below.

The signals at the first IF frequency are then heterodyned in mixer 180b with the 54.0 MHz oscillator signals produced by fixed frequency crystal-controlled oscillator 180c. It was found that it is desirable to crystal-control oscillator 180c to avoid drifts in frequency due to temperature changes which may occur in and around the area of oscillator 180c. While a 54.0 Mhz crystal can be used, it was found that the third overtone (at 54 MHz) of a standard value 18 MHz crystal could be used as well. The result of the heterodyning process is an FM radio signal at the nominal FM IF frequency of 10.7 MHz, which is then filtered in a ceramic resonator arrangement, generally designated 182. The second ceramic resonator of ceramic resonator arrangement 182 was added to improve selectivity. Signals at the output of ceramic resonator arrangement 182 are then amplified, detected, and decoded by FM signal processing units 180d, 180e, and 180f, in the normal manner. A potentiometer VR1 is provided for adjustment of the VCO frequency. Decoded left (L) and right (R) stereo signals are applied to a second pair of input terminals of audio switch 136. When the decoded left (L) and right (R) stereo signals are selected by audio switch unit 136, they are applied to audio amplifier 137 for reproduction in speaker arrangement 138. Lines 117 and 118 coupled between FM radio IC 180 and controller 110 convey signals indicative of whether a signal is tuned, and whether a signal is in stereo, respectively.

Tuner 102 is of the frequency synthesis (FS) type, which means that the frequency of the local oscillator can be changed in a series of steps of a given size under control of controller 100. In FM reception mode, controller 100 causes oscillator 102c to change its frequency in 31.5 kilohertz steps. This means that there can be a mistuning of an FM station by a maximum of 31.5 kHz/2, or 15.75 kHz error. This is acceptable because FM radio IC 180 has acceptable demodulation characteristics over a range of approximately +/- 110 kHz, and also because the FM broadcast frequencies are spaced 200 kHz apart.

The selection of 43.3 MHz as the frequency for the first IF of the double conversion FM radio receiver will now be explained. As is well known, the amplitude vs. frequency characteristic of the tuner is substantially shaped like a haystack, with the chroma carrier and pix carrier residing at respective sides of the haystack approximately 3 db down

from the maximum. The approximate center point of the haystack between these two carriers is 44 Mhz. One skilled in the art might believe that this would be the optimum frequency for the first IF of the FM radio system. However, 44 Mhz is almost exactly the half frequency value of the lowest FM radio frequency (at 88.1 MHz), and would cause the following problem. The frequencies of the signals applied to a mixer are doubled by the action of mixing. Most of these products are out of band and filtered out by tuned circuits coupled to the output of the mixers. If 44 MHz is used as the first IF frequency, then local oscillator 102c would oscillate at 132.1 MHz in order to tune an 88.1 MHz FM carrier. In that case the following signals would be produced,

$$132.1 \text{ MHz} - 88.1 \text{ MHz} = 44 \text{ MHz (the desired signal);}$$

and

$$2 \times 88.1 \text{ MHz} - 132.1 \text{ MHz} = 44.1 \text{ MHz (undesired image).}$$

The undesired image signal is well within the bandwidth of the second IF. This situation causes interference and distortion at the system audio outputs. This is further complicated by the fact that tuner FM traps give very little attenuation at 88.1 MHz causing intermodulation distortion in the tuner to happen at relatively low input signal levels. Frequencies greater than 44 Mhz, but less than the pix carrier at 45.75 MHz, would cause image problems on higher FM radio stations. The best value therefore is one below 44 MHz, but higher than the color carrier at 42.17 MHz (because going lower than the color carrier would cause the signal to drop rapidly down the "haystack"). The value 43.3 MHz is close enough to the crest of the haystack to provide symmetrical signals, and far enough away from 44 MHz to avoid image interference problems. When 43.3 MHz is selected as the first IF frequency, local oscillator 102c would be controlled to oscillate at 132.4 MHz in order to select an FM carrier at 88.1 MHz. this produces the following output signals,

$$132.4 \text{ MHz} - 88.1 \text{ MHz} = 43.3 \text{ MHz (the desired signal);}$$

and

$$2 \times 88.1 \text{ MHz} - 132.4 \text{ MHz} = 44.8 \text{ MHz (undesired image).}$$

The undesired image signal is now 1.5 MHz away from the desired signal, is well outside the 300kHz bandwidth of the second IF stage, and will not cause distortion. In fact, a signal having a frequency between 43.5 MHz and the color subcarrier frequency, is a good candidate for the first IF of the above-described double conversion tuner.

Similarly, the second IF has an image problem to be avoided. Specifically, a signal at 48.65 MHz (i.e., 43.3 MHz +5.35 MHz (one-half the second IF frequency of 10.7 MHz)) would cause an image to appear at 10.7 MHz, again causing interference. Because the second IF frequency is fixed at 10.7 MHz, this problem is eliminated in filter unit 145 without having to employ tracking filters. The circuitry of filter unit 145 is shown in detail in FIGURE 6A. The 43.3 MHz bandpass filter comprises a pi-type arrangement of an inductor L601, and capacitors C601 and C602. A trap at 48.65 Mhz was obtained by adding a capacitor C603 in parallel with inductor L601. The gain vs. frequency characteristic for this arrangement is shown in FIGURE 6B. The following component values are preferred:

L601	101	nanohenries
C601	39	picofarads
C602	120	picofarads
C603	100	picofarads

In operation, controller 110 receives a command, via local keyboard 122, or via IR receiver 120, to enter the FM radio mode. In response, controller 110 applies a signal to the base of transistor Q1 via resistor R1. Transistor Q1 switches on and provides a source of supply voltage to a voltage regulator circuit R2, D2 which in turn provides power (VCC) to operate FM radio IC 180. This switched VCC is also applied to the control terminal of stereo switch 136 and causes the selection the FM radio audio signals in FM radio mode.

There are two obstacles to good FM reception performance, poor sensitivity and overload, and a carefully chosen compromise between the two must be utilized. Recall that in the television mode of operation, the RF amplifier is gain

controlled by an AGC signal derived in the television video IF (VIF) circuitry. In FM mode, the AGC signals are disconnected from the RF amplifier because no meaningful AGC signals are being produced in the VIF circuitry. If the television tuner were to be operated at maximum gain in FM reception mode, medium to strong level FM signals would overdrive the tuner mixer and RF stages, creating unwanted distortion products. Providing a separate FM AGC arrangement is simply unacceptable due to the cost and complexity which would be added to the television receiver. The solution is to operate the RF stage of the tuner at a fixed gain during FM reception mode. This arrangement has a much lower cost, adding only a few components. The gain reduction must be chosen carefully. Too much gain reduction would produce poor FM reception sensitivity, and too little gain reduction yields an overload situation. A second factor which aids to make operation of the RF stage at a reduced gain function well, is the fact that the noise figure of the gain reduced RF amplifier stage is degraded (becomes higher) at a much slower rate than the rate for gain reduction, thus maintaining a better signal to noise ratio. This permits compensation for the RF amplifier gain reduction to be placed in a subsequent IF postamplifier stage, to maintain overall receiver sensitivity.

Disconnecting of the AGC signals is accomplished by applying the 4.7 volt FM radio switched VCC to AGC line 102d via a diode D1. The FM radio VCC supply is well regulated enough to yield gain reductions which fall within acceptable tolerances. It is important to note that the FM radio IC chosen has a wide range of usable operating voltages. The 4.7 volt level was specifically chosen to fit the needs of the television tuner RF gain reduction bias. A resistor R3 isolates the AGC circuitry from the applied VCC. The amplitude of the switched VCC after passing through diode D1 is approximately 4 volts. Applying a fixed 4 volt signal to the AGC control terminal of RF amplifier 102a causes it to operate in a lower gain mode.

The switched FM radio VCC is also applied to the base of SAW filter preamplifier 105 to disable the amplifier and further attenuate unwanted signals at the input of video processing unit 130.

Surprisingly, it was found that an FM trap produces a beneficial effect in a television receiver utilizing a single tuner for receiving both television signals and broadcast FM radio signals. Specifically, the FM trap attenuates the FM radio signals which would otherwise have too great an amplitude at the television tuner input. It is also recognized herein that the FM trap should exhibit a frequency response having relatively sharp "skirts" to minimize interference with signals of adjacent television channels, and having a substantially flat band reject region to provide FM signals having a substantially uniform amplitude throughout the FM radio broadcast band.

Figure 2A shows a parallel resonant FM trap known from the prior art. Series resonant FM traps, and combinations of series and parallel FM traps were also known in the prior art. In each case, however, no effort was made to limit the attenuation of these prior FM traps. Instead, each attempted to obtain the deepest possible notch, because in a television receiver without an FM radio, there is no need to preserve any of the broadcast FM signal spectrum. Figure 2B shows the amplitude vs. frequency characteristic of a parallel resonant circuit, such as shown in FIGURE 2A. This arrangement is unsatisfactory for a combined television and FM system for the following reasons. If the resonant frequency of the circuit of FIGURE 2A were to be set at the center of the FM band of frequencies, then the amplitudes of signals of the individual respective FM broadcast stations would vary greatly at the input of the RF amplifier. It is also unsatisfactory because the roll-off of the characteristic (i.e., the slope of the skirts) is not steep enough to provide enough protection from FM interference for the adjacent television channels.

Turning now to Figure 3A, a three-section FM trap is shown which overcomes the above-noted problems of the prior art FM traps. Section I of the three-section FM trap comprises a parallel arrangement of an inductor L301, a resistor R301, and a capacitor C301. Section I is tuned to 97.5 MHz to make the frequency response of the overall arrangement as uniform as possible. Section II of the three-section FM trap comprises a parallel arrangement of an inductor L302 and capacitor C302. Section II is tuned to 104.0 MHz to provide protection for VHF channels 12 & 13 (in the U. S.). Section III of the three-section FM trap comprises a series resonant circuit disposed from a point between Sections I and II, to a point of reference potential (i.e., signal ground). Section III is tuned to 90.5 MHz to protect low band VHF channel 6 against educational FM transmissions which are as close as 88.1 MHz. Resistors R301 and R303 set the trap depth. It should be noted that Section II needs no additional loading since the loading effects of the antenna filter circuitry which follows it, reduces the trap depth of Section II to the amount desired. The above-described arrangement leaves the channel 6 chroma carrier essentially unmodified in level, but pulls down the channel 6 sound carrier about 3-4 db, which is felt to be acceptable. The cable channel A-2 (i.e., 98) picture (pix) carrier is reduced by approximately 1 db, but this too is felt to be acceptable.

The following component values are preferred.

Section I	L301	approx. 18.3 nanohenries (adjust.)
	R301	270 ohms
	C301	150 picofarads
	L302	approx. 16.2 nanohenries (adjust.)

(continued)

Section II	C302	150 picofarads
Section III	L303	approx. 680 microhenries (adjust.)
	R303	6.8 ohms
	C303	4.7 picofarads

The above-described three-section FM trap provides a uniform level of rejection to signals in the 88 MHz to 108 MHz range of approximately 10 +/- 4 db. during the FM reception mode of operation. When the tuner is tuned to channel 6, however, the FM band rejections, as shown in FIGURE 3B, are in the range of 18-22 db due to the added selectivity of the antenna input circuitry. The response characteristic shown in FIGURE 3B was measured at the drain terminal of the RF amplifier dual-gate FET transistor Q501 of FIGURE 5.

The three-section FM trap described above exhibits the following typical performance (referenced against the broadcast television channel pix carrier).

Frequency (MHz)	Response (db)
83.25 (chan 6 pix ref.)	- 0
86.83 (chan 6 chroma)	-0.2
87.75 (chan 6 sound)	-2.7
88.1 (lowest FM station)	-4.6
88.3	-5.4
88.5	-6.2
88.7	-7.1
88.9	-8.0
89.1	-9.0
90.1	-12.6
90.5	-12.2
91.1	-10.1
92.1	-8.2
93.1	-7.6
94.1	-8.0
95.1	-9.0
96.1	-10.3
97.1	-11.1
98.1	-10.8
99.1	-9.9
100.1	-9.0
101.1	-8.7
102.1	-9.2
103.1	-10.7
104.1	-11.8
105.1	-7.8
106.1	-3.3
107.1	-0.8
107.9 (top FM station)	-0.4

The desired end result of the trap attenuations by themselves, is that a required reduction of overall tuner gain at the FM band of frequencies is achieved. Compared to the average power gain of adjacent television channels 6 and 98, the reduction of the overall tuner gain at the following FM band frequencies is realized.

FREQUENCY (MHz)	TYPICAL AVERAGE LOSS RELATIVE TO THE AVERAGE POWER GAIN OF ADJACENT TELEVISION CHANNELS 6 AND 98 (db)
88.1	7.5
90.5	13
93.5	12
97.5	12
100.7	10.5
104.1	6.5
107.9	0

During FM reception mode no television images are available for viewing. Accordingly, when an FM station is selected controller 110 causes on-screen display processor 140 to display a message indicating to a user that the television receiver is in FM mode, that a particular FM station has been selected and whether or not the received FM signal is in stereo. Such a display is shown in FIGURE 4, wherein a message is displayed on the screen 410 of a television receiver 400. The display is presented to the user for a predetermined period of time (perhaps 30 seconds), after which there is displayed a blank screen.

FIGURE 5 shows in detail the connection of the FM trap circuit of FIGURE 3A to a simplified version of a portion of tuner 102. Specifically, the output of FM trap 500 is coupled through a series inductor, to a series of traps, generally designated 510. Traps 510 have a first parallel trap tuned to the TV IF frequency, a second shunt series trap to remove all signals below channel 2, and a second parallel trap also tuned to the TV IF frequency. The output of traps 510 is applied to the input of RF amplifier, generally designated 520. A tuner of this type is known from the MTP-M2016 tuner used with the CTC-156 chassis manufactured by Thomson Consumer Electronics, Inc., Indianapolis, Indiana, USA, and does not need to be described in detail.

It is also recognized herein that the subject apparatus can be used to tune broadcasts of information services, such as, in the United States, the National Weather Service (NWS). These broadcasts are allocated to the following seven frequencies: 162.400 MHz, 162.425 MHz, 162.450 MHz, 162.475 MHz, 162.500 MHz, 162.525 MHz, and 162.550 MHz. Only one of these frequencies is assigned to a given geographic area. Typical weather radio receivers provide a switch for selecting one of three crystal controlled frequencies for receiving the broadcast.

It is further recognized herein that when NWS mode is selected only the center of the NWS band need be tuned. This is true for three reasons. First, the IF filters have a 190 kHz 3db bandwidth which is greater than the 150 kHz total channel spacing of the NWS band. Second, the discriminator used performs well, even +/- 1000 kHz from the tuned frequency. Third, there is little or no overlap of the NWS stations (because the NWS frequencies are reserved, and because there is only one transmitter operating in a given area).

It is herein specifically recognized that the subject invention is also useful in videocassette recorders (VCRs). The term television receiver, as used herein, includes television receivers having a video display device (commonly known as television sets) and television receivers without a video display device, such as VCRs.

Claims

1. A television receiver comprising:

tuner means (102) for operating in a first mode for receiving television RF signals, said tuner means (102) selecting a particular television RF signal from a plurality of television RF signals in response to a control signal; said tuner means (102) also operating in a second mode as a first frequency conversion stage for a double conversion broadcast FM radio RF signal, said tuner means selecting a particular broadcast FM radio RF signal from a plurality of broadcast FM radio RF signals in response to said control signal, and for converting said particular broadcast FM radio RF signal to a first intermediate frequency; control means (104) for generating said control signal for causing said tuner means to select one of said particular television RF signal and said particular broadcast FM radio RF signal; and **characterized by** a second frequency conversion stage (180b, 180c) of said double conversion broadcast FM radio signal receiver, said second frequency conversion stage (180b, 180c) exclusively receiving said broadcast FM radio signal at said first intermediate frequency and converting said broadcast FM radio signal at said first intermediate frequency to a second intermediate frequency, said second intermediate frequency being other than a television intercarrier sound intermediate frequency; and

means (130e) for demodulating audio signals from said broadcast FM radio signal at said second intermediate frequency.

2. The television receiver of claim 1, characterized in that said second intermediate frequency is 10.7 MHz.
3. The television receiver of claim 2, characterized in that said second frequency conversion stage (180b, 180c) is an element of an FM radio receiver integrated circuit.

4. A television receiver, comprising:

tuner means (102) for operating in a first mode for receiving television RF signals, said tuner means (102) selecting a particular television RF signal from a plurality of television RF signals in response to a control signal and converting said selected RF signal to a television intermediate frequency (IF) signal; means (130) for demodulating said television IF signal to produce a television audio signal; control means (104) for generating said control signal for causing said tuner means to select said particular RF signal; said tuner means (102) also operating in a second mode as a first frequency conversion stage for a double conversion FM stereo radio signal receiver, for converting an FM stereo signal to a first intermediate frequency; and characterized by a second frequency conversion stage (180b, 180c) of said double conversion FM radio signal receiver, said second frequency conversion stage (180b, 180c) exclusively receiving said FM stereo signal at said first intermediate frequency and converting said FM stereo signal to a second intermediate frequency; means (180e) for demodulating audio signals from said FM stereo signal at said second intermediate frequency and to produce demodulated FM stereo audio signals; and means (136) for selecting for amplification and reproduction one of said television audio signal and said demodulated FM stereo audio signals.

Patentansprüche

1. Fernsehempfänger umfassend:

Tunermittel (102) zum Arbeiten in einer ersten Betriebsart zum Empfang von HF-Fernsehsignalen, wobei die Tunermittel (102) ein bestimmtes HF-Fernsehsignal aus einer Vielzahl von HF-Fernsehsignalen in Abhängigkeit von einem Steuersignal auswählen; wobei die Tunermittel (102) auch in einer zweiten Betriebsart als erste Mischstufe für ein Doppel-Überlagerungs-FM-Rundfunk-HF-Signal arbeiten, wobei die Tunermittel ein bestimmtes FM-Rundfunk-HF-Signal aus einer Vielzahl von FM-Rundfunk-HF-Signalen in Abhängigkeit von dem Steuersignal auswählen, und um das bestimmte FM-Rundfunk-HF-Signal in eine erste Zwischenfrequenz umzuwandeln; Steuermittel (104) zur Erzeugung des Steuersignals, um zu bewirken, daß die Tunermittel das bestimmte HF-Fernsehsignal und das bestimmte FM-Rundfunk-HF-Signal auswählen; und gekennzeichnet durch: eine zweite Mischstufe (180b, 180c) des Doppel-Überlagerungs-FM-Rundfunksignalempfängers, wobei die zweite Mischstufe (180b, 180c) ausschließlich das FM-Rundfunksignal mit der ersten Zwischenfrequenz empfängt und das FM-Rundfunksignal mit der ersten Zwischenfrequenz in eine zweite Zwischenfrequenz umwandelt, wobei die zweite Zwischenfrequenz anders als eine Fernseh-Zwischenträger-Ton-Zwischenfrequenz ist, und Mittel (180e) zur Demodulation von Audiosignalen von dem FM-Rundfunksignal mit der zweiten Zwischenfrequenz.

2. Fernsehempfänger nach Anspruch 1, dadurch gekennzeichnet, daß die zweite Zwischenfrequenz 10,7 MHz beträgt.
3. Fernsehempfänger nach Anspruch 2, dadurch gekennzeichnet, daß die zweite Mischstufe (180b, 180c) ein Element einer integrierten FM-Rundfunkempfängerschaltung ist.
4. Fernsehempfänger umfassend:

Tunermittel (102) zum Arbeiten in einer ersten Betriebsart zum Empfang von HF-Fernsehsignalen, wobei die

Tunermittel (102) ein bestimmtes HF-Fernsehsignal aus einer Vielzahl von HF-Fernsehsignalen in Abhängigkeit von einem Steuersignal auswählen und das ausgewählte HF-Signal in ein Fernseh-Zwischenfrequenz-Signal (IF) umwandelt;

Mittel (130) zum Demodulieren des Fernseh-ZF-Signals, um ein Fernseh-Audiosignal zu erzeugen;

Steuermittel (104) zur Erzeugung des Steuersignals, um zu bewirken, daß die Tunermittel das bestimmte HF-Signal auswählen;

wobei die Tunermittel (102) auch in einer zweiten Betriebsart als erste Mischstufe für einen Doppel-Überlagerungs-FM-Rundfunk-Stereosignal-Empfänger arbeiten, um ein FM-Stereosignal in eine erste Zwischenfrequenz umzuwandeln; gekennzeichnet durch:

eine zweite Mischstufe (180b, 180c) des Doppel-Überlagerungs-FM-Rundfunksignalempfängers, wobei die zweite Mischstufe (180b, 180c) ausschließlich das FM-Stereosignal mit der ersten Zwischenfrequenz empfängt und das FM-Stereosignal in eine zweite Zwischenfrequenz umwandelt;

Mittel (180e) zum Demodulieren von Audiosignalen von dem FM-Stereosignal mit der zweiten Zwischenfrequenz und zum Erzeugen von demodulierten FM-Stereo-Audiosignalen; und

Mittel (136) zum Auswählen entweder des Fernseh-Audiosignals oder der demodulierten FM-Stereo-Audiosignale für die Verstärkung und Wiedergabe.

Revendications

1. Récepteur de télévision intégrant :

un moyen syntoniseur (102) fonctionnant dans un premier mode de réception de signaux RF de télévision, ledit moyen syntoniseur (102) sélectionnant un signal RF de télévision particulier dans un ensemble de signaux RF de télévision en réponse à un signal de commande ;

ledit moyen syntoniseur (102) fonctionnant également dans un second mode comme premier étage à double changement de fréquence pour délivrer un signal RF de radiodiffusion en MF à double changement de fréquence, ledit syntoniseur sélectionnant un signal RF de radiodiffusion en MF spécifique dans un ensemble de signaux RF de radiodiffusion en MF en réponse audit signal de commande, et convertissant ledit signal RF de radiodiffusion en MF particulière à une première fréquence intermédiaire,

un moyen de commande (104) permettant de générer ledit signal de commande pour que ledit moyen syntoniseur sélectionne l'un desdits signaux RF de télévision particuliers et dudit signal RF de radiodiffusion en MF particulier et **caractérisé par**

un second étage à double changement de fréquence (180b, 180c) dudit récepteur de signaux de radiodiffusion en MF à double changement de fréquence, ledit second étage à double changement de fréquence (180b, 180c) recevant exclusivement ledit signal de radiodiffusion en MF à ladite première fréquence intermédiaire et convertissant ledit signal de radiodiffusion en MF à ladite première fréquence intermédiaire en une seconde fréquence intermédiaire, ladite seconde fréquence intermédiaire n'étant pas une fréquence intermédiaire son interporteuse de télévision ; et

un moyen (180e) de démodulation des signaux audio à partir dudit signal de radiodiffusion en MF à ladite seconde fréquence intermédiaire.

2. Récepteur de télévision selon la revendication 1, caractérisé en que ladite seconde fréquence intermédiaire est de 10,7 MHz.

3. Récepteur de télévision de la Revendication 2, caractérisé en ce que ledit second étage à double changement de fréquence (180b, 180c) fait partie d'un circuit intégré du récepteur radio MF.

4. Récepteur de télévision intégrant :

un moyen syntoniseur (102) fonctionnant dans un premier mode pour la réception des signaux RF de télévision, ledit moyen syntoniseur (102) sélectionnant un signal RF de télévision spécifique dans un ensemble de signaux RF de télévision en réponse à un signal de commande, et convertissant ledit signal RF sélectionné en un signal de télévision à fréquence intermédiaire (FI) ;

un moyen (130) de démodulation dudit signal FI de télévision servant à générer un signal audio de télévision;

un moyen de commande (104) générant ledit signal de commande afin que ledit moyen syntoniseur sélectionne ledit signal RF particulier ;

ledit moyen syntoniseur (102) fonctionnant également dans un second mode comme premier étage à double

changement de fréquence pour un récepteur de signaux radio stéréo MF à double changement de fréquence, en vue de la conversion d'un signal stéréo MF en une première fréquence intermédiaire ; et caractérisé par ; un second étage à double changement de fréquence (180b, 180c) dudit récepteur de signaux radio MF à double changement de fréquence, ledit second étage à double changement de fréquence (180b, 180c) recevant exclusivement ledit signal stéréo MF à ladite première fréquence intermédiaire, et convertissant ledit signal stéréo MF en une seconde fréquence intermédiaire.

un moyen (180e) de démodulation des signaux audio à partir dudit signal stéréo MF, à ladite seconde fréquence intermédiaire, et de génération de signaux audio stéréo MF démodulés; et

un moyen (136) de sélection en vue de l'amplification et la restitution de l'un desdits signaux de télévision et desdits signaux audio stéréo MF démodulés.

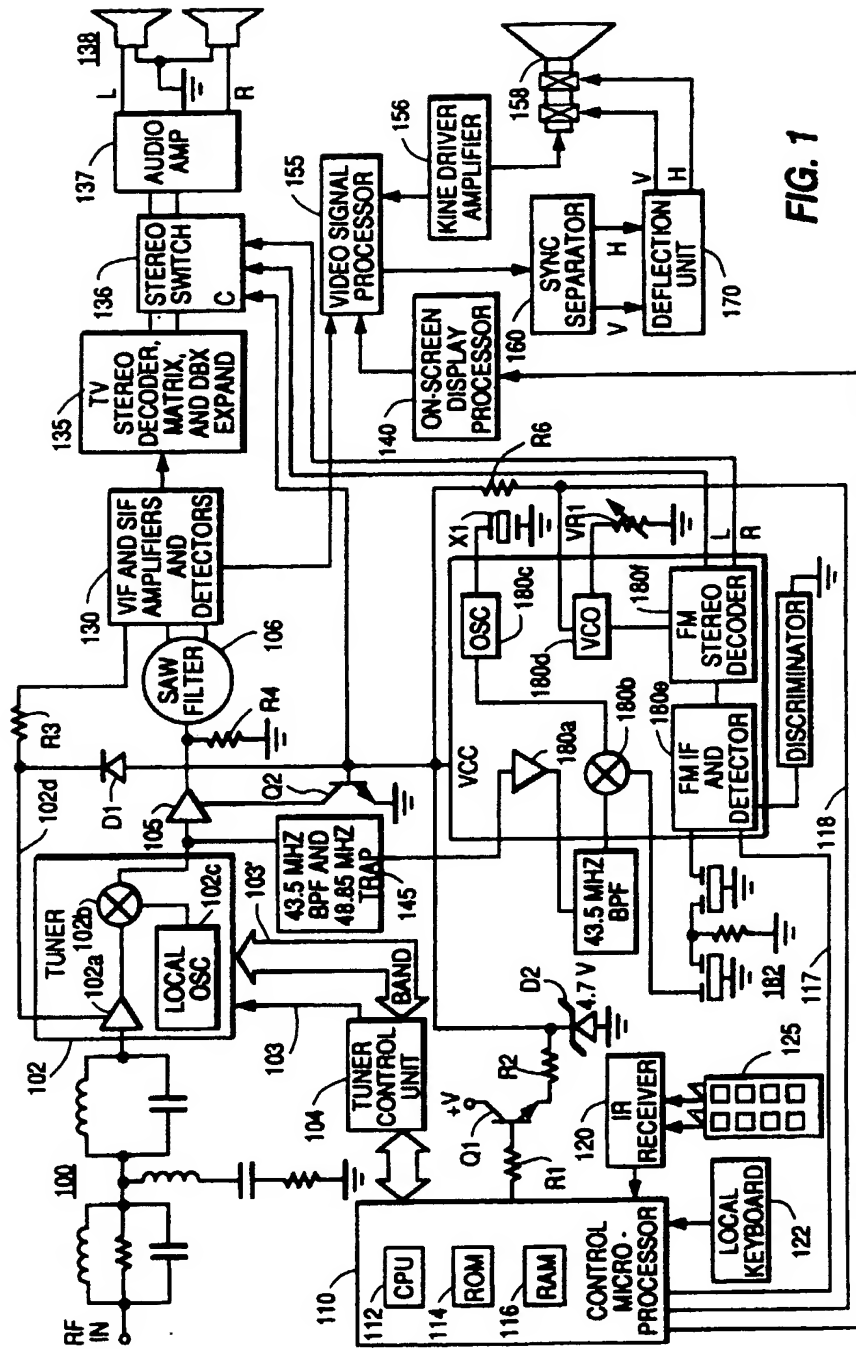


FIG. 1



FIG. 2A
PRIOR ART

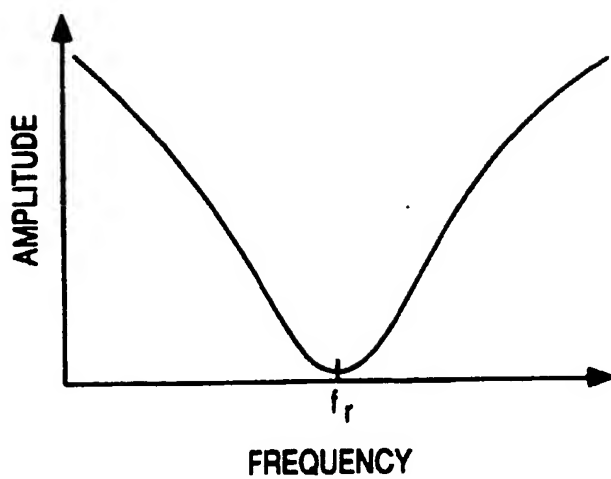


FIG. 2B
PRIOR ART

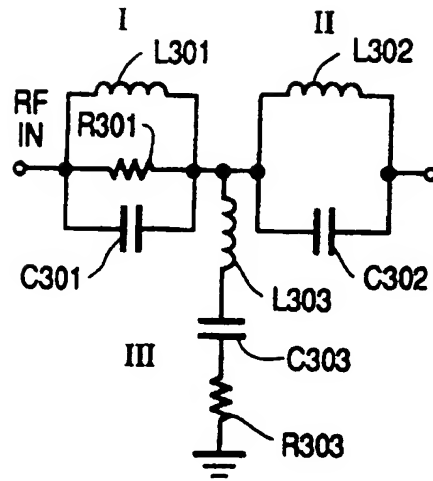


FIG. 3A

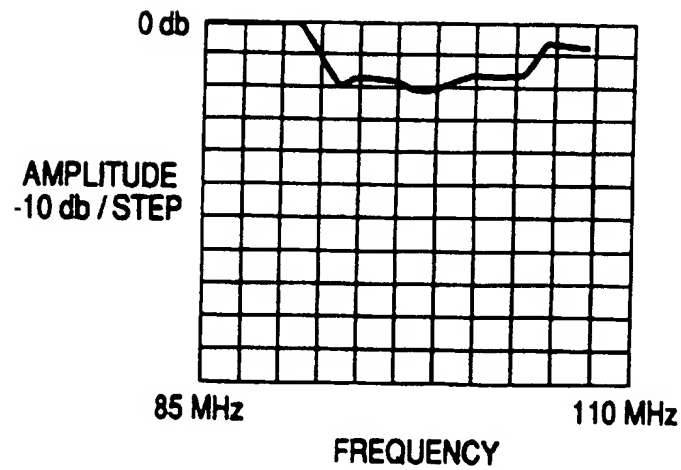


FIG. 3B

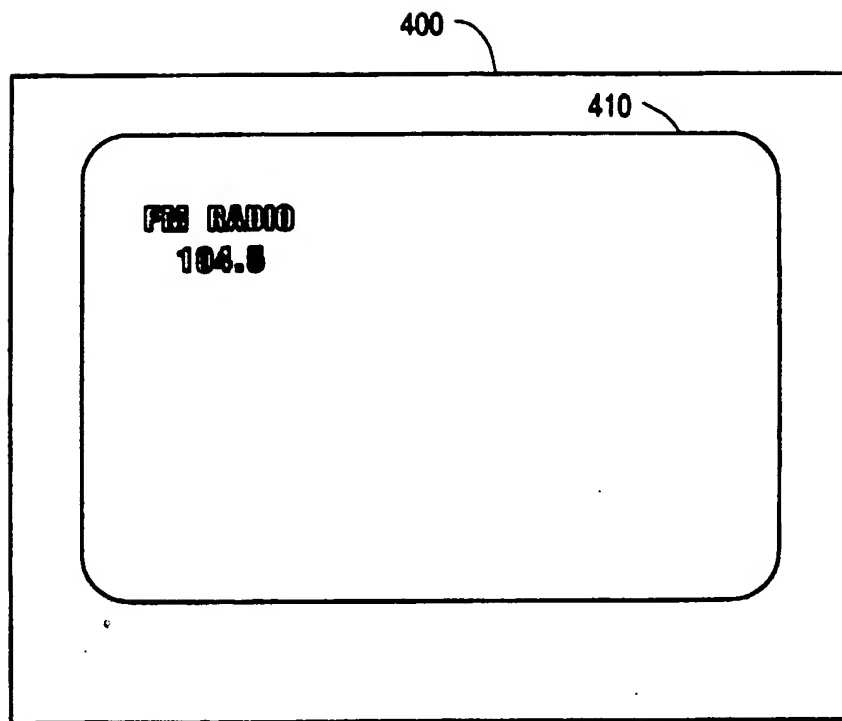
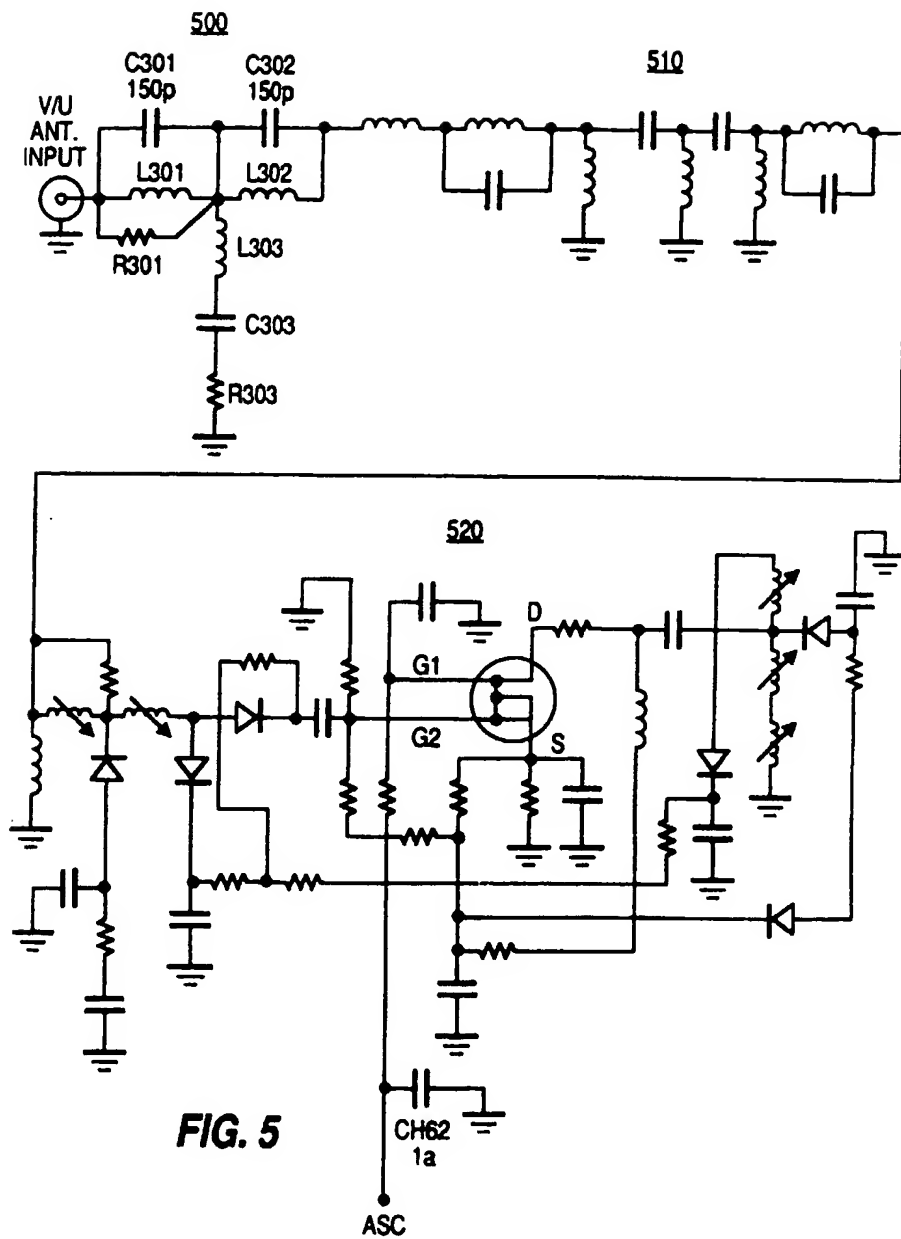


FIG. 4



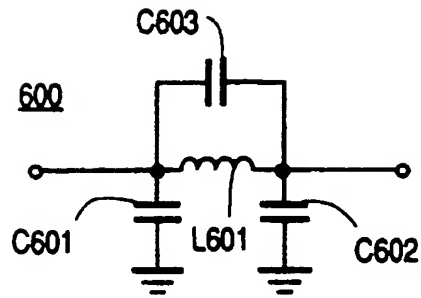


FIG. 6A

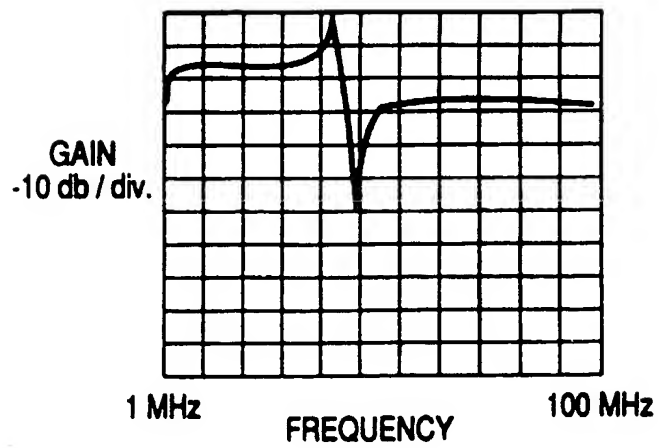
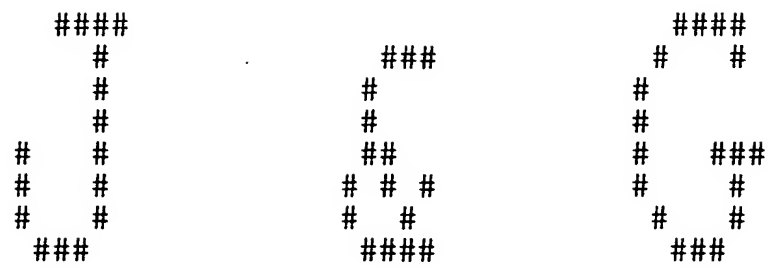
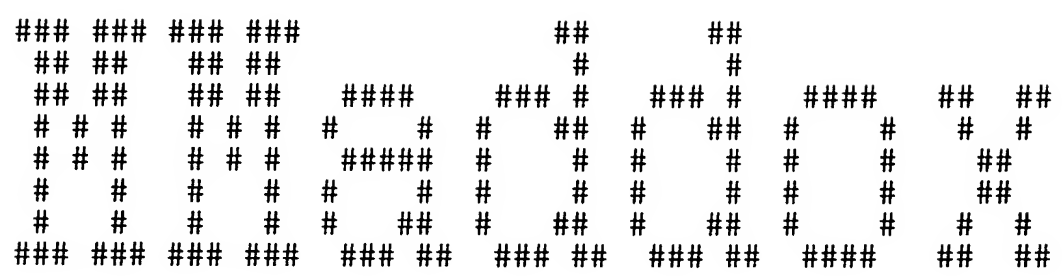


FIG. 6B



Print Job For:



Spooled By: MMaddox
Job Number: 202
Date Printed: 2/24/2005
Time Printed: 7:34:51 PM



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(54) **Information radio reception in a television receiver by synthesizing only center frequency**

**Rundfunkinformationsempfang in einem Fernsehempfänger durch alleinige Synthese der
Zentralfrequenz**

**Réception d'information radio dans un récepteur de télévision par synthèse de la seule fréquence
centrale**

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(E-149)17 December 1982 & JP-A-57 155 885

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Description

Field of the Invention.

5 The subject application concerns the field of television receivers including an FM radio.

Background of the Invention

10 It is desirable to have a television receiver which is capable of receiving not only television signals, but also broadcast FM radio signals. In the United States, the broadcast FM band occupies a band of frequencies extending from approximately 88 MHz to approximately 108 MHz. This band of frequencies lies between the frequencies allocated for broadcast television channel 6 and television cable channel 98. Television receivers having the capability to receive broadcast FM signals are known from the prior art. However, in these known arrangements, their respective manufacturers added a separate FM-radio having its own tuner. It is also known from the prior art to combine a television receiver and an information receiver, such as, for example, in the United States, a National Weather Service (NWS) radio receiver. However, in this case as well, the respective manufacturers included a separate tuner for tuning NWS signals.

20 National Weather Service receiver, sometimes called "weather radios", typically include three crystals, each of which is tuned to a different Weather Service frequency. Each of the three crystals is user-selectable by a switch, for changing the operating frequency of the radio to that of the nearest National Weather Service transmitter. It is noted that the National Weather Service has seven frequencies allocated to it, not three. It is also noted that a large area of the country may not be covered by transmitters operating on a frequency corresponding to one of the three normally provided crystals. If a weather radio or other information service is to be combined with a television receiver, it is desirable that a user be able to receive National Weather Service messages in all areas of the country. It is also desirable that the user does not have to operate switches to find the proper operating frequency.

25 In the US-A-4,688,263 a dual conversion AM-FM radio receiver is disclosed in which AM and FM broadcast RF signals from a first IF amplifier are converted by a mixer to a second intermediate frequency. The arrangement allows a high integration density for integrating into an integrated circuit.

30 Combined television and FM radio receivers which in part use common circuitry are known for instance from JP-55085174 and JP57155885.

SUMMARY OF THE INVENTION

35 A single tuner in a television receiver is employed for tuning television signals in at least one band of television frequencies, and broadcast FM radio signals in an FM band of frequencies adjacent to the television band of frequencies. The television tuner serves as the first frequency conversion stage of a double conversion FM receiver, wherein an FM radio integrated circuit serves as the second frequency conversion stage. It is herein recognized that the tuner can be controlled to tune the center frequency of an information service such as the National Weather Service band of frequencies, and such tuning is all that is necessary to automatically receive National Weather Service signals on any of the seven allocated frequencies, because the total bandwidth of the National Weather Service band is less than the bandwidth of the second IF of the double conversion FM radio tuner.

BRIEF DESCRIPTION OF THE DRAWING

45 FIGURE 1 shows, in block diagram form, a television receiver incorporating the subject invention.

FIGURE 2A shows a parallel resonant FM trap as known from the prior art.

FIGURE 2B is a graph of the amplitude vs. frequency characteristic of a parallel resonant circuit of the type shown in FIGURE 2A.

FIGURE 3A shows an FM trap in accordance with the subject invention.

50 FIGURE 3B is a graph of the amplitude vs. frequency characteristic of the FM trap of FIGURE 3A and antenna input circuitry, when the tuner is tuned to channel 6.

FIGURE 4 is an illustration showing a display screen produced in accordance with the invention.

FIGURE 5 is an illustration of a portion of the tuner of FIGURE 1, showing the connection of the FM trap of FIGURE 3A.

55 FIGURE 6 shows the combined 43.3 MHz bandpass filter and 48.65 MHz half-IF trap of FIGURE 1.

DETAILED DESCRIPTION OF THE EMBODIMENT

Referring to FIGURE 1, television radio frequency (RF) and broadcast FM radio frequency signals are applied to an RF input terminal of an FM trap circuit generally designated 100. FM trap 100 will be described in detail below with respect to FIGURE 3. RF signals appearing at the output of FM trap 100 are applied to a tuner 102. Tuner 102 includes an RF amplifier 102a for amplifying RF signals, and applying the amplified RF signals to one input of a mixer 102b. Tuner 102 also includes a local oscillator 102c for generating a local oscillator signal which when applied to a second input of mixer 102b heterodynes with the amplified RF signal and produces an output signal at the television intermediate frequency (IF frequency). Tuner 102 selects a particular RF signal under control of a tuner control unit 104. Alternatively, tuner control unit 104 may also be included within tuner 102. Tuner control unit 104 applies a tuning control signal to tuner 102 via a wire 103, and applies bandswitching signals via a control bus 103'. The tuning control signal and bandswitching signals control the frequency at which local oscillator 102c oscillates, thus determining which RF signal is converted (heterodyned) to the IF frequency. Tuner control unit 104 is controlled by a controller 110. Controller 110, which may be a microprocessor or microcomputer, includes a central processing unit (CPU) 112, a read-only memory (ROM) 114, and a random access memory 116. Controller 110 receives user-entered control signals from a local keyboard 122, and from an infrared (IR) receiver 120. IR receiver 120 receives and decodes remote control signals transmitted by a remote control unit 125.

The intermediate frequency (IF) signal produced by tuner 102 is applied to a surface acoustic wave (SAW) filter preamplifier 105 which amplifies the IF signal and applies it, via SAW filter 106 to a video signal processing unit 130. Video signal processing unit 130 comprises a video IF (VIF) amplifying stage, an automatic gain control circuit (AGC), an automatic fine tuning circuit (AFT), a video detector, and a sound IF (SIF) amplifying stage. Processing unit 130 produces a baseband composite video signal (TV), and a sound carrier signal. The sound carrier signal is applied to an audio signal processor unit 135 which includes a TV stereo decoder, a matrix, and a DBX expander. Audio signal processor unit 135 produces left and right audio signals and applies them to one pair of inputs of an audio switch unit 136. The output of audio switch unit 136 is coupled to an audio amplifier unit 137. Audio amplifier unit 137 produces amplified baseband left and right audio signals and applies them to a pair of speakers 138 for sound reproduction.

The baseband video signal (TV) is coupled to a video processor unit 155 and a kine driver amplifier 156, and ultimately displayed on a display screen of a display device 158. Video signals are also applied to a sync separator unit 160 which derives vertical and horizontal synchronizing signals therefrom. The derived vertical and horizontal signals are applied to a deflection unit 170 for the production of deflection signals for application to the yoke assembly of display device 158. Under control of controller 110, an on-screen display processor 140 generates character signals, and applies them to a second input of video signal processor 155, for display on display device 158. The circuitry described thus far, with the exception of the particular FM trap shown in FIGURE 1, is known from the RCA CTC 156 color television chassis.

The intermediate frequency (IF) signal produced by tuner 102 is also applied, via a 43.3 Mhz bandpass filter and 48.65 MHz trap arrangement 145, to a single chip FM radio integrated circuit (IC) 180. FM radio IC 180 is, for example, a CXA12338M/S AM/FM Stereo Radio Circuit manufactured by SONY Corporation. FM radio IC 180 includes an amplifier 180a, a mixer 180b, an oscillator 180c, a voltage controlled oscillator (VCO) 180d, an FM IF and detector unit 180e, and an FM stereo decoder unit 180f.

It is herein recognized that television tuner 102 may be used as the first frequency conversion stage of a double conversion tuner for the FM broadcast band, wherein the second frequency conversion stage of the double conversion tuner is provided by FM radio IC 180. That is, a particular FM radio signal is selected and converted in frequency from one of the FM radio band of frequencies, to a first intermediate frequency of 43.3 MHz. The value 43.3 MHz is important and its selection will be discussed below.

The signals at the first IF frequency are then heterodyned in mixer 180b with the 54.0 MHz oscillator signals produced by fixed frequency crystal-controlled oscillator 180c. It was found that it is desirable to crystal-control oscillator 180c to avoid drifts in frequency due to temperature changes which may occur in and around the area of oscillator 180c. While a 54.0 Mhz crystal can be used, it was found that the third overtone (at 54 MHz) of a standard value 18 MHz crystal could be used as well. The result of the heterodyning process is an FM radio signal at the nominal FM IF frequency of 10.7 MHz, which is then filtered in a ceramic resonator arrangement, generally designated 182. The second ceramic resonator of ceramic resonator arrangement 182 was added to improve selectivity. Signals at the output of ceramic resonator arrangement 182 are then amplified, detected, and decoded by FM signal processing units 180d, 180e, and 180f, in the normal manner. A potentiometer VR1 is provided for adjustment of the VCO frequency. Decoded left (L) and right (R) stereo signals are applied to a second pair of input terminals of audio switch 136. When the decoded left (L) and right (R) stereo signals are selected by audio switch unit 136, they are applied to audio amplifier 137 for reproduction in speaker arrangement 138. Lines 117 and 118 coupled between FM radio IC 180 and controller 110 convey signals indicative of whether a signal is tuned, and whether a signal is in stereo, respectively.

Tuner 102 is of the frequency synthesis (FS) type, which means that the frequency of the local oscillator can be

changed in a series of steps of a given size under control of controller 100. In FM reception mode, controller 100 causes oscillator 102c to change its frequency in 31.5 kilohertz steps. This means that there can be a mistuning of an FM station by a maximum of 31.5 kHz/2, or 15.75 kHz error. This is acceptable because FM radio IC 130 has acceptable demodulation characteristics over a range of approximately +/- 110 kHz, and also because the FM broadcast frequencies are spaced 200 kHz apart.

The selection of 43.3 MHz as the frequency for the first IF of the double conversion FM radio receiver will now be explained. As is well known, the amplitude vs. frequency characteristic of the tuner is substantially shaped like a haystack, with the chroma carrier and pix carrier residing at respective sides of the haystack approximately 3 db down from the maximum. The approximate center point of the haystack between these two carriers is 44 MHz. One skilled in the art might believe that this would be the optimum frequency for the first IF of the FM radio system. However, 44 MHz is almost exactly the half frequency value of the lowest FM radio frequency (at 88.1 MHz), and would cause the following problem. The frequencies of the signals applied to a mixer are doubled by the action of mixing. Most of these products are out of band and filtered out by tuned circuits coupled to the output of the mixers. If 44 MHz is used as the first IF frequency, then local oscillator 102c would oscillate at 132.1 MHz in order to tune an 88.1 MHz FM carrier. In that case the following signals would be produced,

$$132.1 \text{ MHz} - 88.1 \text{ MHz} = 44 \text{ MHz}$$

(the desired signal); and

$$2 \times 88.1 \text{ MHz} - 132.1 \text{ MHz} = 44.1 \text{ MHz}$$

(undesired image).

The undesired image signal is well within the bandwidth of the second IF. This situation causes interference and distortion at the system audio outputs. This is further complicated by the fact that tuner FM traps give very little attenuation at 88.1 MHz causing intermodulation distortion in the tuner to happen at relatively low input signal levels. Frequencies greater than 44 MHz, but less than the pix carrier at 45.75 MHz, would cause image problems on higher FM radio stations. The best value therefore is one below 44 MHz, but higher than the color carrier at 42.17 MHz (because going lower than the color carrier would cause the signal to drop rapidly down the "haystack"). The value 43.3 MHz is close enough to the crest of the haystack to provide symmetrical signals, and far enough away from 44 MHz to avoid image interference problems. When 43.3 MHz is selected as the first IF frequency, local oscillator 102c would be controlled to oscillate at 132.4 MHz in order to select an FM carrier at 88.1 MHz. this produces the following output signals,

$$132.4 \text{ MHz} - 88.1 \text{ MHz} = 43.3 \text{ MHz}$$

(the desired signal); and

$$2 \times 88.1 \text{ MHz} - 132.4 \text{ MHz} = 44.8 \text{ MHz}$$

(undesired image).

The undesired image signal is now 1.5 MHz away from the desired signal, is well outside the 300kHz bandwidth of the second IF stage, and will not cause distortion. In fact, a signal having a frequency between 43.5 MHz and the color subcarrier frequency, is a good candidate for the first IF of the above-described double conversion tuner.

Similarly, the second IF has an image problem to be avoided. Specifically, a signal at 48.65 MHz (i.e., 43.3 MHz +5.35 MHz (one-half the second IF frequency of 10.7 MHz)) would cause an image to appear at 10.7 MHz, again causing interference. Because the second IF frequency is fixed at 10.7 MHz, this problem is eliminated in filter unit 145 without having to employ tracking filters. The circuitry of filter unit 145 is shown in detail in FIGURE 6A. The 43.3 MHz bandpass filter comprises a pi-type arrangement of an inductor L601, and capacitors C601 and C602. A trap at 48.65 MHz was obtained by adding a capacitor C603 in parallel with inductor L601. The gain vs. frequency characteristic for this arrangement is shown in FIGURE 6B. The following component values are preferred:

L601	101 nanohenries
C601	39 picofarads
C602	120 picofarads
C603	100 picofarads

In operation, controller 110 receives a command, via local keyboard 122, or via IR receiver 120, to enter the FM radio mode. In response, controller 110 applies a signal to the base of transistor Q1 via resistor R1. Transistor Q1 switches on and provides a source of supply voltage to a voltage regulator circuit R2, D2 which in turn provides power (VCC) to operate FM radio IC 180. This switched VCC is also applied to the control terminal of stereo switch 136 and causes the selection the FM radio audio signals in FM radio mode.

There are two obstacles to good FM reception performance, poor sensitivity and overload, and a carefully chosen compromise between the two must be utilized. Recall that in the television mode of operation, the RF amplifier is gain controlled by an AGC signal derived in the television video IF (VIF) circuitry. In FM mode, the AGC signals are disconnected from the RF amplifier because no meaningful AGC signals are being produced in the VIF circuitry. If the television tuner were to be operated at maximum gain in FM reception mode, medium to strong level FM signals would overdrive the tuner mixer and RF stages, creating unwanted distortion products. Providing a separate FM AGC arrangement is simply unacceptable due to the cost and complexity which would be added to the television receiver. The solution is to operate the RF stage of the tuner at a fixed gain during FM reception mode. This arrangement has a much lower cost, adding only a few components. The gain reduction must be chosen carefully. Too much gain reduction would produce poor FM reception sensitivity, and too little gain reduction yields an overload situation. A second factor which aids to make operation of the RF stage at a reduced gain function well, is the fact that the noise figure of the gain reduced RF amplifier stage is degraded (becomes higher) at a much slower rate than the rate for gain reduction, thus maintaining a better signal to noise ratio. This permits compensation for the RF amplifier gain reduction to be placed in a subsequent IF postamplifier stage, to maintain overall receiver sensitivity.

Disconnecting of the AGC signals is accomplished by applying the 4.7 volt FM radio switched VCC to AGC line 102d via a diode D1. The FM radio VCC supply is well regulated enough to yield gain reductions which fall within acceptable tolerances. It is important to note that the FM radio IC chosen has a wide range of usable operating voltages. The 4.7 volt level was specifically chosen to fit the needs of the television tuner RF gain reduction bias. A resistor R3 isolates the AGC circuitry from the applied VCC. The amplitude of the switched VCC after passing through diode D1 is approximately 4 volts. Applying a fixed 4 volt signal to the AGC control terminal of RF amplifier 102a causes it to operate in a lower gain mode.

The switched FM radio VCC is also applied to the base of SAW filter preamplifier 105 to disable the amplifier and further attenuate unwanted signals at the input of video processing unit 130.

Surprisingly, it was found that an FM trap produces a beneficial effect in a television receiver utilizing a single tuner for receiving both television signals and broadcast FM radio signals. Specifically, the FM trap attenuates the FM radio signals which would otherwise have too great an amplitude at the television tuner input. It is also recognized herein that the FM trap should exhibit a frequency response having relatively sharp "skirts" to minimize interference with signals of adjacent television channels, and having a substantially flat band reject region to provide FM signals having a substantially uniform amplitude throughout the FM radio broadcast band.

Figure 2A shows a parallel resonant FM trap known from the prior art. Series resonant FM traps, and combinations of series and parallel FM traps were also known in the prior art. In each case, however, no effort was made to limit the attenuation of these prior FM traps. Instead, each attempted to obtain the deepest possible notch, because in a television receiver without an FM radio, there is no need to preserve any of the broadcast FM signal spectrum. Figure 2B shows the amplitude vs. frequency characteristic of a parallel resonant circuit, such as shown in FIGURE 2A. This arrangement is unsatisfactory for a combined television and FM system for the following reasons. If the resonant frequency of the circuit of FIGURE 2A were to be set at the center of the FM band of frequencies, then the amplitudes of signals of the individual respective FM broadcast stations would vary greatly at the input of the RF amplifier. It is also unsatisfactory because the roll-off of the characteristic (i.e., the slope of the skirts) is not steep enough to provide enough protection from FM interference for the adjacent television channels.

Turning now to Figure 3A, a three-section FM trap is shown which overcomes the above-noted problems of the prior art FM traps. Section I of the three-section FM trap comprises a parallel arrangement of an inductor L301, a resistor R301, and a capacitor C301. Section I is tuned to 97.5 MHz to make the frequency response of the overall arrangement as uniform as possible. Section II of the three-section FM trap comprises a parallel arrangement of an inductor L302 and capacitor C302. Section II is tuned to 104.0 MHz to provide protection for VHF channels 12 & 13 (in the U. S.). Section III of the three-section FM trap comprises a series resonant circuit disposed from a point between Sections I and II, to a point of reference potential (i.e., signal ground). Section III is tuned to 90.5 MHz to protect low band VHF channel 6 against educational FM transmissions which are as close as 88.1 MHz. Resistors R301 and R303 set the trap depth. It should be noted that Section II needs no additional loading since the loading effects of the antenna filter circuitry which follows it, reduces the trap depth of Section II to the amount desired. The above-described arrangement leaves the channel 6 chroma carrier essentially unmodified in level, but pulls down the channel 6 sound carrier about 3-4 db, which is felt to be acceptable. The cable channel A-2 (i.e., 98) picture (pix) carrier is reduced by approximately 1 db, but this too is felt to be acceptable.

The following component values are preferred.

Section I	L301	approx. 18.3 nanohenries (adjust.)
	R301	270 ohms
	C301	150 picofarads
Section II	L302	approx. 16.2 nanohenries (adjust.)
	C302	150 picofarads
Section III	L303	approx. 680 microhenries (adjust.)
	R303	6.8 ohms
	C303	4.7 picofarads

The above-described three-section FM trap provides a uniform level of rejection to signals in the 88 MHz to 108 MHz range of approximately 10 +/- 4 db. during the FM reception mode of operation. When the tuner is tuned to channel 6, however, the FM band rejections, as shown in FIGURE 3B, are in the range of 18-22 db due to the added selectivity of the antenna input circuitry. The response characteristic shown in FIGURE 3B was measured at the drain terminal of the RF amplifier dual-gate FET transistor Q501 of FIGURE 5.

The three-section FM trap described above exhibits the following typical performance (referenced against the broadcast television channel pix carrier).

	<u>Frequency (MHz)</u>	<u>Response (db)</u>
	83.25 (chan 6 pix ref.)	- 0
5	86.83 (chan 6 chroma)	-0.2
	87.75 (chan 6 sound)	-2.7
	88.1 (lowest FM station)	-4.6
10	88.3	-5.4
	88.5	-6.2
	88.7	-7.1
	88.9	-8.0
15	89.1	-9.0
	90.1	-12.6
	90.5	-12.2
20	91.1	-10.1
	92.1	-8.2
	93.1	-7.6
25	94.1	-8.0
	95.1	-9.0
	96.1	-10.3
30	97.1	-11.1
	98.1	-10.8
	99.1	-9.9
35	100.1	-9.0
	101.1	-8.7
	102.1	-9.2
	103.1	-10.7
40	104.1	-11.8
	105.1	-7.8
	106.1	-3.3
45		
	107.1	-0.8
	107.9 (top FM station)	-0.4

50 The desired end result of the trap attenuations by themselves, is that a required reduction of overall tuner gain at the FM band of frequencies is achieved. Compared to the average power gain of adjacent television channels 6 and 98, the reduction of the overall tuner gain at the following FM band frequencies is realized.

55	<u>FREQUENCY (MHz)</u>	<u>TYPICAL AVERAGE LOSS RELATIVE TO THE AVERAGE POWER GAIN OF ADJACENT TELEVISION CHANNELS 6 AND 98 (db)</u>
	88.1	7.5
	90.5	13

(continued)

FREQUENCY (MHz)	TYPICAL AVERAGE LOSS RELATIVE TO THE AVERAGE POWER GAIN OF ADJACENT TELEVISION CHANNELS 6 AND 98 (db)
93.5	12
97.5	12
100.7	10.5
104.1	6.5
107.9	0

During FM reception mode no television images are available for viewing. Accordingly, when an FM station is selected controller 110 causes on-screen display processor 140 to display a message indicating to a user that the television receiver is in FM mode, that a particular FM station has been selected and whether or not the received FM signal is in stereo. Such a display is shown in FIGURE 4, wherein a message is displayed on the screen 410 of a television receiver 400. The display is presented to the user for a predetermined period of time (perhaps 30 seconds), after which there is displayed a blank screen.

FIGURE 5 shows in detail the connection of the FM trap circuit of FIGURE 3A to a simplified version of a portion of tuner 102. Specifically, the output of FM trap 500 is coupled through a series inductor, to a series of traps, generally designated 510. Traps 510 have a first parallel trap tuned to the TV IF frequency, a second shunt series trap to remove all signals below channel 2, and a second parallel trap also tuned to the TV IF frequency. The output of traps 510 is applied to the input of RF amplifier, generally designated 520. A tuner of this type is known from the MTP-M2016 tuner used with the CTC-156 chassis manufactured by Thomson Consumer Electronics, Inc., Indianapolis, Indiana, USA, and does not need to be described in detail.

As used herein, NWS is exemplary of an information service. It is also recognized herein that the subject apparatus can be used to tune broadcasts of the National Weather Service (NWS). These broadcasts are allocated to the following seven frequencies: 162.400 MHz, 162.425 MHz, 162.450 MHz, 162.475 MHz, 162.500 MHz, 162.525 MHz, and 162.550 MHz. Only one of these frequencies is assigned to a given geographic area. Typical weather radio receivers provide a switch for selecting one of three crystal controlled frequencies for receiving the broadcast.

It is further recognized herein that when NWS mode is selected only the center of the NWS band need be tuned. This is true for three reasons. First, the IF filters have a 190 kHz 3db bandwidth which is greater than the 150 kHz total channel spacing of the NWS band. Second, the discriminator used performs well, even +/- 1000 kHz from the tuned frequency. Third, there is little or no overlap of the NWS stations (because the NWS frequencies are reserved, and because there is only one transmitter operating in a given area).

It is herein specifically recognized that the subject invention is also useful in videocassette recorders (VCRs). The term television receiver, as used herein, includes television receivers having a video display device (commonly known as television sets) and television receivers without a video display device, such as VCRs.

Claims

1. A television receiver, comprising:

tuner means (102) for operating in a first mode for receiving television RF signals, said tuner means (102) selecting a particular television RF signal from a plurality of television RF signals in response to a control signal (103);

control means (104) for generating said control signal (103) for causing said tuner means (102) to select said particular RF signal; and characterized by

said tuner means (102) also operating in a second mode as a first frequency conversion stage for a double conversion broadcast FM radio signal receiver, for converting signals of said FM signals to a first intermediate frequency;

a second frequency conversion stage (180a, 180b) of said double conversion broadcast FM radio signal receiver, said second frequency conversion stage receiving said signals at said first intermediate frequency and converting said signals to a second intermediate frequency; and

means (180d, 180e) for demodulating audio signals from said signals at said second intermediate frequency; said double conversion FM signal receiver also being tuned by said control means (104) substantially to the center of the band of frequencies of an information service, said FM signal receiver automatically receiving signals broadcast on any one of the frequencies of said band of an information service frequencies.

2. The television receiver of claim 1, characterized in that said second intermediate frequency is 10.7 MHz.
3. The television receiver of claim 2, characterized in that said second frequency conversion stage (180a, 180b) is an element of an FM radio receiver integrated circuit.
4. The television receiver of claim 1, characterized in that said band of information service frequencies includes the frequencies 162.400 MHz and 162.550 MHz.
5. The television receiver of claim 4, characterized in that said tuner means (102) is tuned, in said second mode of operation, to said center of said information service band of frequencies, said center being approximately 162.475 MHz, said tuning of said tuner means to said center being sufficient to automatically receive broadcasts at each of said frequencies in said band.

Patentansprüche

1. Fernsehempfänger umfassend:

Tuner-Mittel (102) für das Arbeiten in einer ersten Betriebsart zum Empfang von Fernseh-HF-Signalen, wobei die Tuner-Mittel (102) ein besonderes Fernseh-HF-Signal aus einer Vielzahl von Fernseh-HF-Signalen in Abhängigkeit von einem Steuersignal (103) auswählen; Steuermittel (104) zum Erzeugen des Steuersignals (103), um die Tuner-Mittel (102) zu veranlassen, das besondere HF-Signal auszuwählen, dadurch gekennzeichnet, daß die Tuner-Mittel (102) auch in einer zweiten Betriebsart als erste Mischstufe für einen Doppel-Überlagerungs-FM-HF-Signalempfänger arbeiten, um Signale der FM-Signale in eine erste Zwischenfrequenz umzuwandeln; eine zweite Mischstufe (180a, 180b) des Doppel-Überlagerungs-FM-HF-Signalempfängers vorgesehen ist, die die Signale mit der ersten Zwischenfrequenz empfängt und die Signale in eine zweite Zwischenfrequenz umwandelt; und Mittel (180d, 180e) zum Demodulieren von Audiosignalen von den Signalen mit der zweiten Zwischenfrequenz vorgesehen sind; der Doppel-Überlagerungs-FM-HF-Signalempfänger auch durch die Steuermittel (104) auf etwa die Mitte des Frequenzbandes eines Informationsdienstes abgestimmt wird, wobei der FM-Signalempfänger automatisch Signale empfängt, die auf einer der Frequenzen des Frequenzbandes eines Informationsdienstes gesendet werden.

2. Fernsehempfänger nach Anspruch 1, dadurch gekennzeichnet, daß die zweite Zwischenfrequenz 10,7 MHz ist.
3. Fernsehempfänger nach Anspruch 2, dadurch gekennzeichnet, daß die zweite Mischstufe (180a, 180b) ein Element einer integrierten Schaltung eines FM-Rundfunkempfängers ist.
4. Fernsehempfänger nach Anspruch 1, dadurch gekennzeichnet, daß das Band von Informationsdienst-Frequenzen die Frequenzen 162,400 MHz und 162,550 MHz enthält.
5. Fernsehempfänger nach Anspruch 4, dadurch gekennzeichnet, daß die Tuner-Mittel (102) in der zweiten Betriebsart auf die Mitte des Informationsdienst-Frequenzbandes abgestimmt werden, daß die Mitte etwa 162,475 MHz beträgt, wobei die Abstimmung der Tuner-Mittel auf die Mitte ausreicht, um automatisch Sendungen auf jeder der Frequenzen in dem Band zu empfangen.

Revendications

1. Récepteur télévision comprenant :

un dispositif de réglage (102) utilisable sur un premier mode pour recevoir les signaux de télévision HF, ledit dispositif de réglage (102) sélectionnant un signal télévision HF spécifique à partir d'un ensemble de signaux télévision HF en réponse à un signal de commande (103) ;
un dispositif de commande (104) servant à générer ledit signal de commande (103) pour permettre audit dispositif de réglage (102) de sélectionner ledit signal HF spécifique ; **et caractérisé par :**
ledit dispositif de réglage (102) fonctionnant également sur un second mode correspondant à un premier étage

de conversion de fréquence destiné à un récepteur de signaux radio FM à double conversion (pour convertir les signaux desdits signaux FM en une première fréquence intermédiaire) ;

un deuxième étage de conversion de fréquence (180a, 180b) dudit récepteur de signaux radio FM à double conversion, ledit second étage de conversion de fréquence recevant lesdits signaux à ladite première fréquence intermédiaire et convertissant lesdits signaux en une seconde fréquence intermédiaire ; et

des dispositifs (180d, 180e) servant à démoduler les signaux audio desdits signaux à ladite seconde fréquence intermédiaire, et

ledit récepteur de signal FM à double conversion étant également réglé via ledit dispositif de commande (104) effectivement au centre de la bande de fréquences d'un service d'informations, ledit récepteur de signal FM recevant automatiquement des signaux diffusés sur une des fréquences de ladite bande de fréquences d'un service d'informations.

2. Récepteur télévision selon la Revendication 1, caractérisé en ce que ladite fréquence intermédiaire est réglée sur 10,7 MHz.

3. Récepteur télévision selon la Revendication 2, caractérisé en ce que ledit second étage de conversion de fréquences (180a, 180b) est un élément de circuit intégré pour récepteur radio FM.

4. Récepteur de télévision selon la Revendication 1, caractérisé en ce que ladite bande de fréquences de service d'informations inclut les fréquences 162,400 MHz et 162,550 MHz.

5. Récepteur télévision selon la Revendication 4, caractérisé en ce que ledit dispositif de réglage (102) est accordé, dans ledit second mode d'utilisation, sur ledit centre de ladite bande de fréquences du service d'informations, ledit centre étant réglé approximativement sur 162,475 MHz, ledit réglage dudit dispositif de réglage sur ledit centre étant suffisant pour recevoir automatiquement les diffusions sur chacune desdites fréquences de ladite bande.

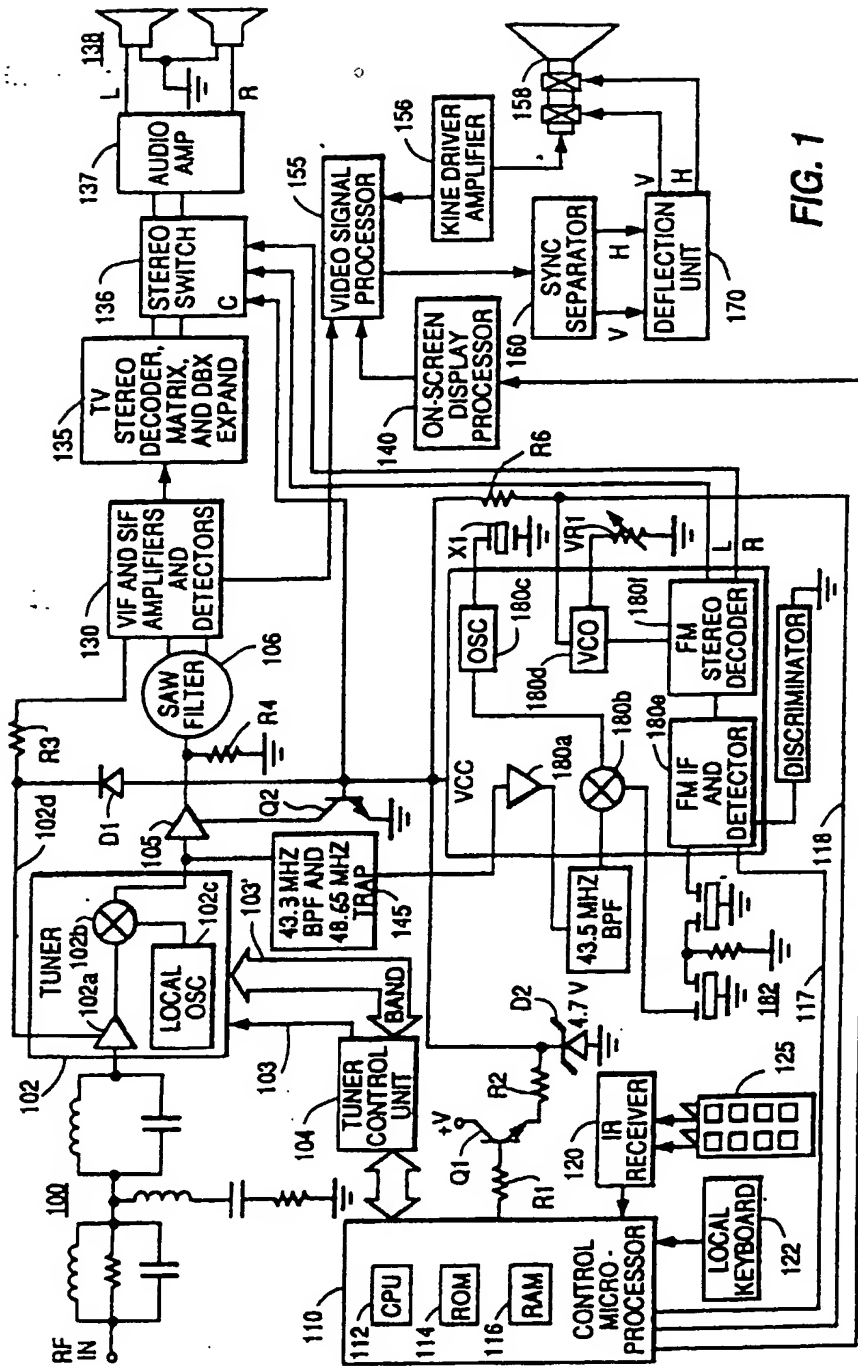


FIG. 1

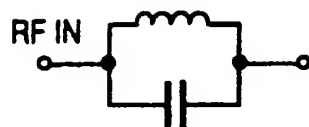


FIG. 2A
PRIOR ART

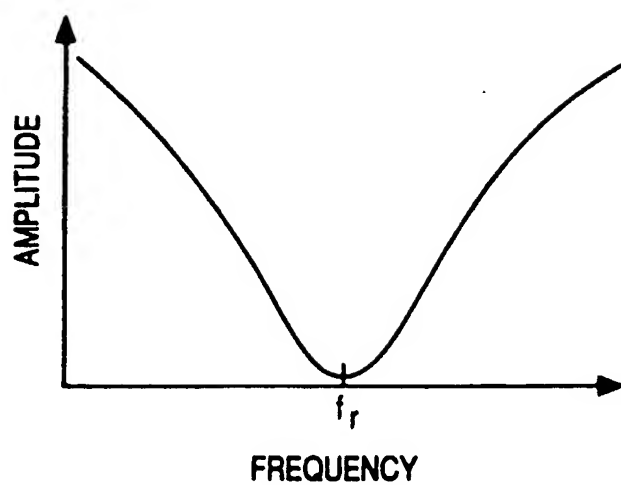


FIG. 2B
PRIOR ART

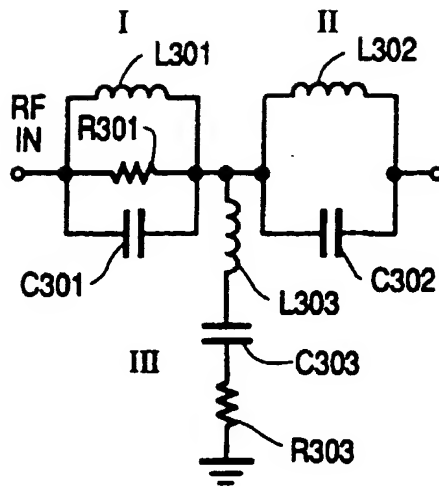


FIG. 3A

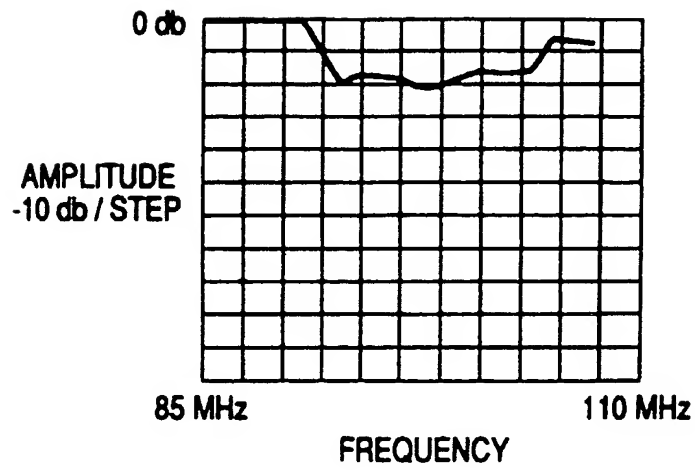


FIG. 3B

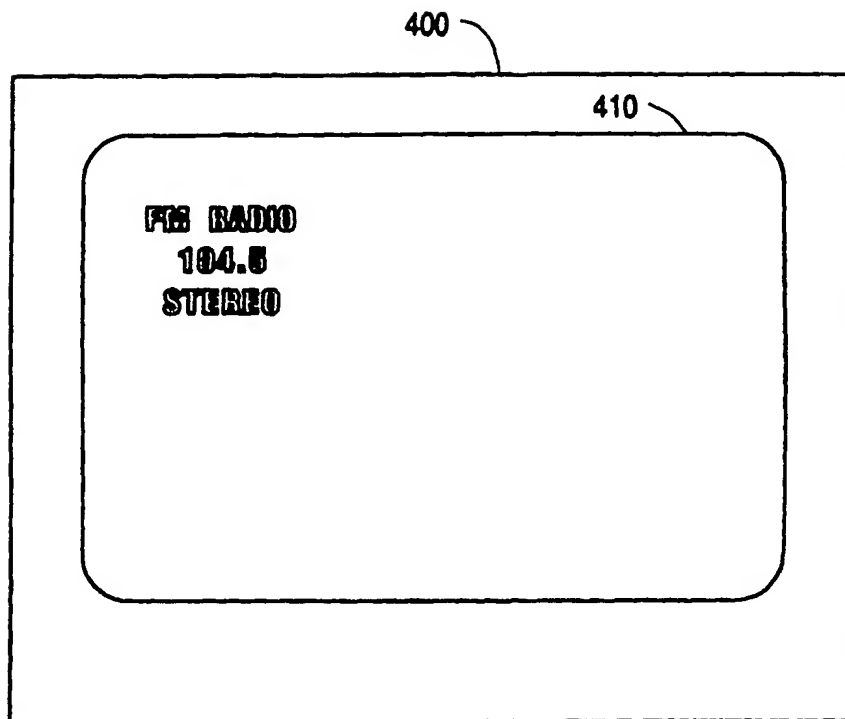
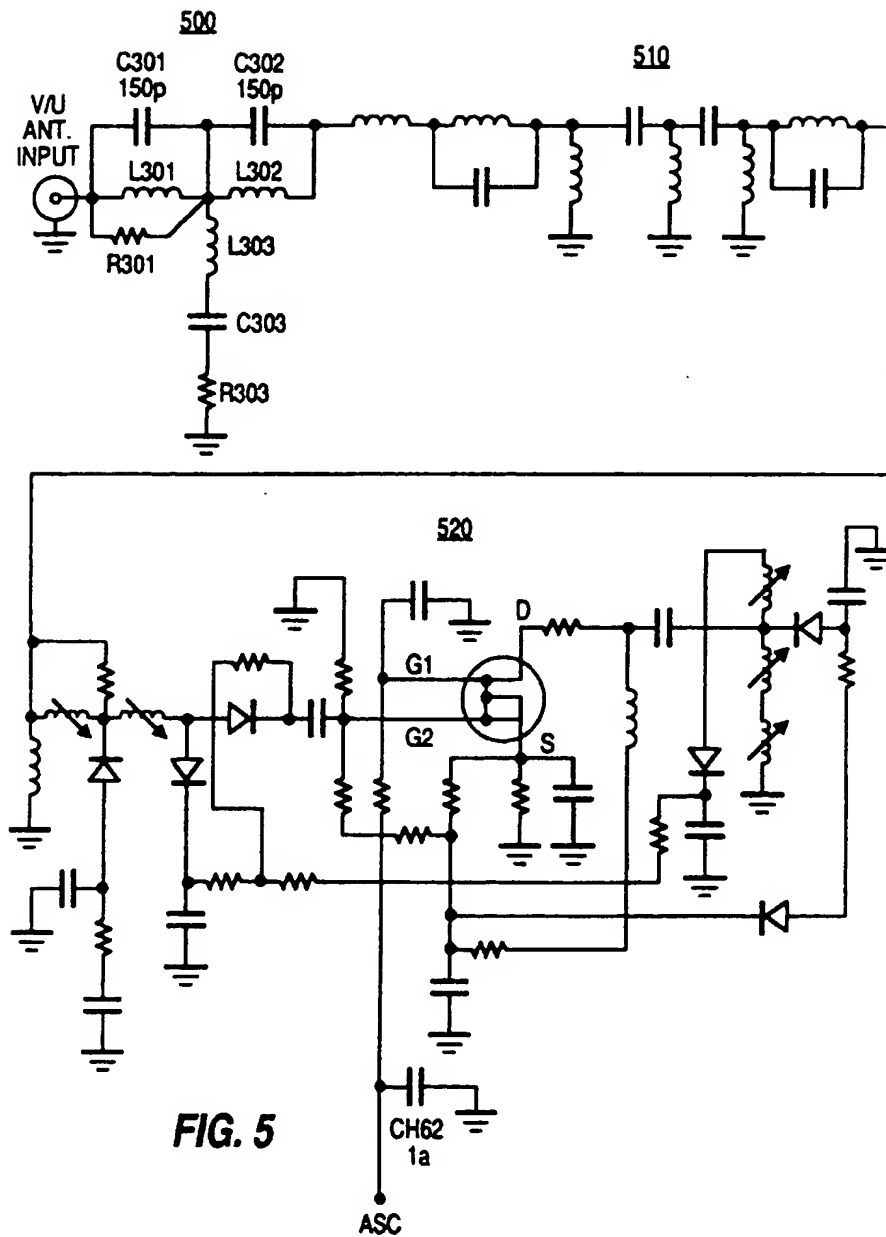


FIG. 4



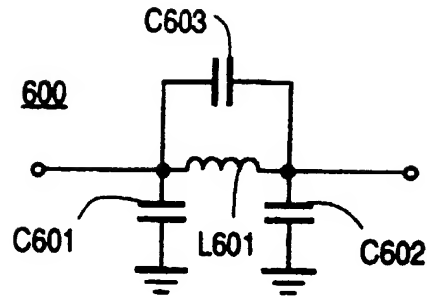


FIG. 6A

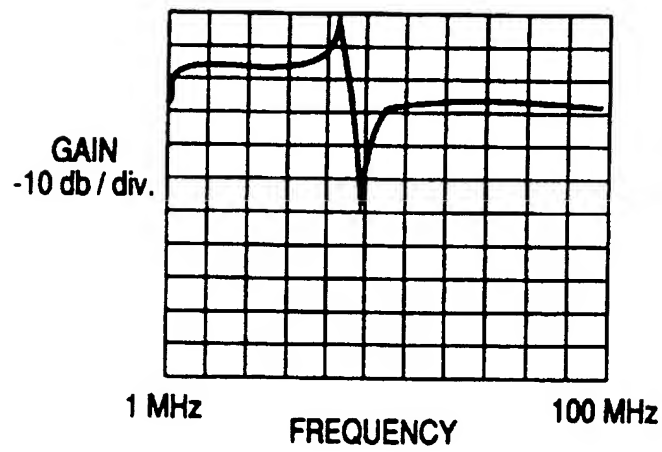


FIG. 6B

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